

$$f(x_{i+1}) = f(x_i) + f'(x_i)h + f''(x_i)\frac{h^2}{2} + O(h^3) \quad (1)$$

$$f(x_{i+2}) = f(x_i) + f'(x_i)(2h) + f''(x_i)\frac{(2h)^2}{2} + O(h^3) \quad (2)$$

(a) To eliminate $f'(x_i)$ terms subtract 2 times Eqn (1) from Eqn (2)

$$f(x_{i+2}) - 2f(x_{i+1}) = -f(x_i) + f''(x_i)\left[\frac{4h^2}{2} - \frac{2h^2}{2}\right] + O(h^3)$$

$$\Rightarrow f''(x_i)h^2 = f(x_{i+2}) - 2f(x_{i+1}) + f(x_i) + O(h^3)$$

$$\Rightarrow \boxed{f''(x_i) = \frac{f(x_{i+2}) - 2f(x_{i+1}) + f(x_i)}{h^2} + O(h)}$$

(b) To eliminate $f''(x_i)$ terms subtract 4 times Eqn (1) from Eqn (2)

$$f(x_{i+2}) - 4f(x_{i+1}) = -3f(x_i) + f'(x_i)(2h - 4h) + O(h^3)$$

$$\Rightarrow f'(x_i)2h = -f(x_{i+2}) + 4f(x_{i+1}) - 3f(x_i) + O(h^3)$$

$$\Rightarrow \boxed{f'(x_i) = \frac{-f(x_{i+2}) + 4f(x_{i+1}) - 3f(x_i)}{2h} + O(h^2)}$$

3.2

- Eliminate f_i'' , f_i''' , and $f_i^{(4)}$ terms
- Subtracting the first two equations and the last two equations will eliminate f_i'' and f_i''' in each and leave two equations with f_i' and $f_i^{(4)}$. Then $f_i^{(4)}$ can be eliminated from those two equations.

• Eqn (1b) - Eqn (2b)

$$f_{i+1} - f_{i-1} = 2hf_i' + \frac{h^3}{3}f_i^{(4)} + o(h^5) \quad (5b)$$

• Eqn (3b) - Eqn (4b)

$$f_{i+2} - f_{i-2} = 4hf_i' + \frac{8}{3}h^3f_i^{(4)} + o(h^5) \quad (6b)$$

• $8 \times$ Eqn (5b) - Eqn (6b)

$$8f_{i+1} - 8f_{i-1} - f_{i+2} + f_{i-2} = 12hf_i' + o(h^5)$$

Solve for f_i'

$$f_i' = \frac{(f_{i-2} - 8f_{i-1} + 8f_{i+1} - f_{i+2})}{12h} + o(h^4)$$

Want an expression for f_i'' → must
manipulate the given equations to eliminate
all other derivatives.

Step 1 Eq. (1) + Eq. (2) (Eliminate odd power derivatives)

$$\Rightarrow f_{i+1} + f_{i-1} = 2f_i + h^2 f_i'' + \frac{h^4}{12} f_i^{(4)} + o(h^6) \quad (5)$$

Step 2 Eq. (3) + Eq. (4) (Eliminate odd power derivatives)

$$f_{i+2} + f_{i-2} = 2f_i + 4h^2 f_i'' + \frac{4}{3} h^4 f_i^{(4)} + o(h^6) \quad (6)$$

Step 3 Eliminate $f_i^{(4)}$ derivatives between Eq. (5) & Eq. (6)

$$16 * \text{Eq. (5)} - \text{Eq. (6)}$$

$$16 f_{i+1} + 16 f_{i-1} - f_{i+2} - f_{i-2} = 32 f_i + 16 h^2 f_i'' + \frac{16}{12} h^4 f_i^{(4)} - 2 f_i - 4 h^2 f_i'' - \frac{16}{12} h^4 f_i^{(4)} + o(h^6)$$

$$\Rightarrow 16 f_{i+1} + 16 f_{i-1} - f_{i+2} - f_{i-2} = 30 f_i + 12 h^2 f_i'' + o(h^6)$$

$$\Rightarrow f_i'' = \frac{-f_{i-2} + 16 f_{i-1} - 30 f_i + 16 f_{i+1} - f_{i+2} + o(h^6)}{12 h^2}$$

$$f_i'' = \frac{-f_{i-2} + 16 f_{i-1} - 30 f_i + 16 f_{i+1} - f_{i+2}}{12 h^2} + o(h^4)$$

3.4

3-4-1

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$$f(x) = \frac{1}{x}$$

$$f'(x) = -\frac{1}{x^2}$$

$$f''(x) = \frac{2}{x^3}$$

predict $f(5)$ using a base point at $x = 4$.

True Value: $f(5) = \frac{1}{5} = 0.2$

$$x_i = 4$$

$$x_{i+1} = 5$$

$$h = 1$$

Zero order

$$f(x_{i+1}) = f(x_i)$$

$$f(5) = \frac{1}{4} = 0.25 \quad \leftarrow$$

$$\epsilon_t = \frac{0.2 - 0.25}{0.2} \times 100\% = -25\% \quad \leftarrow$$

first order

$$f(x_{i+1}) = f(x_i) + f'(x_i)h$$

$$f(5) = \frac{1}{4} + \left(-\frac{1}{4^2}\right)1 = 0.1875 \quad \leftarrow$$

$$\epsilon_t = \frac{0.2 - 0.1875}{0.2} \times 100\% = +6.25\% \quad \leftarrow$$

second order

$$f(x_{i+1}) = f(x_i) + f'(x_i)h + f''(x_i)\frac{h^2}{2}$$

$$f(5) = \frac{1}{4} + \left(-\frac{1}{4^2}\right)1 + \left(\frac{2}{4^3}\right)\frac{1^2}{2}$$

$$f(5) = 0.203125 \quad \leftarrow$$

$$\epsilon_t = \frac{0.2 - 0.203125}{0.2} \times 100\% = -1.56\% \quad \leftarrow$$

$$f(x) = \ln x$$

$$f'(x) = \frac{1}{x}$$

$$f''(x) = -\frac{1}{x^2}$$

2nd order Taylor series expansion

$$f(x+h) = f(x) + hf'(x) + \frac{h^2}{2}f''(x)$$

Approximate $f(5)$ from a base point of $x=3$:

- base point $x=3$
- spacing: $h=2$

- exact value $f(5) = \ln 5 = 1.60944$

Approximation: $f(5) \approx \ln 3 + 2\left(\frac{1}{3}\right) + \frac{(2)^2}{2} \left(\frac{-1}{(3)^2}\right)$

$$f(5) \approx 1.09861 + 0.666667 - 0.222222$$

$$f(5) \approx 1.54306$$

$$E_t = \frac{(1.60944 - 1.54306)}{1.60944} \times 100 = \underline{4.12\%}$$

3.6

3-6-1

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Use standard finite difference equations in one dimension for the partial derivative.

$$\theta^*(x^*, t^*) = [C_1 \exp(-\xi_1^2 t^*)] \cos(\xi_1 x^*)$$

$$C_1 = 1.0472 \quad t^* = 5.0$$

$$\xi_1 = 0.5 \text{ (rad)}$$

Backward Difference (First Order)

Jaluria pg 84 $f_i' = \frac{(f_i - f_{i-1})}{\Delta x}$

in this nomenclature

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{x^*=1, \text{ 1st order, BD}} = \frac{\theta^*(1, t^*) - \theta^*(1 - \Delta x^*, t^*)}{\Delta x^*}$$

In all cases $[C_1 \exp(-\xi_1^2 t^*)]$ is constant

$$[C_1 \exp(-\xi_1^2 t^*)] = [1.0472 \exp(-0.5^2 \cdot 5.0)] = 0.30003$$

Step size $\Delta x^* = 0.2$

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{x^*=1, \Delta x^*=0.2} = \frac{\theta^*(1, 5) - \theta^*(0.8, 5)}{0.2}$$

$$\theta^*(1, 5) = 0.3003 \cos(0.5(1)) = 0.263301$$

$$\theta^*(0.8, 5) = 0.3003 \cos(0.5(0.8)) = 0.276346$$

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{x^*=1, \Delta x^*=0.2} = \frac{0.263301 - 0.276346}{0.2} = -0.065225 \leftarrow$$

CONTINUED

3.6 (continued)

• Step size $\Delta x^* = 0.1$

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{\substack{x^*=1 \\ \Delta x^*=0.1}} = \frac{\theta^*(1, 5) - \theta^*(0.9, 5)}{0.1}$$

$$\theta^*(0.9, 5) = 0.30003 \cos(0.5(0.9)) = 0.270161$$

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{\substack{x^*=1 \\ \Delta x^*=0.1}} = \frac{0.263301 - 0.270161}{0.1} = -0.068600 \quad \leftarrow$$

Exact Solution

$$\begin{aligned} \left. \frac{\partial \theta^*}{\partial x^*} \right|_{x^*=1} &= \left[c_1 \exp(-\xi_1^2 t^*) \right] \left. \frac{\partial (\cos(\xi_1 x^*))}{\partial x^*} \right|_{x^*=1} \\ &= 0.30003 \left[-\xi_1 \sin(\xi_1 x^*) \right]_{x^*=1} \end{aligned}$$

$$= -0.30003 (0.5) \sin(0.5) = -0.0719210$$

Errors

$$\Delta x^* = 0.2 : \epsilon_t = \frac{(-0.0719210 - (-0.065225))}{-0.0719210} \times 100\% = \underline{9.31\%}$$

$$\Delta x^* = 0.1 : \epsilon_t = \frac{-0.0719210 - (-0.068600)}{-0.0719210} \times 100\% = \underline{4.62\%}$$

$$\theta(x) = \frac{\cosh[m(L-x)]}{\cosh[mL]}$$

$$m = 150.0 \text{ (m}^{-1}\text{)}$$

$$L = 0.3 \text{ (m)}$$

$$\cosh[u] = \frac{1}{2}(e^u + e^{-u}) \quad \text{or directly available in a calculator}$$

$$\frac{d\theta}{dx} = \frac{d}{dx} \left(\frac{\cosh[m(L-x)]}{\cosh[mL]} \right) = \frac{-m \sinh[m(L-x)]}{\cosh[mL]}$$

First derivative forward difference approximation of $\frac{d\theta}{dx}$ is

$$\frac{d\theta}{dx} \approx \frac{\theta_{x+\Delta x} - \theta_x}{\Delta x}$$

$$\Delta x = 0.05 \text{ (m)}$$

$$\frac{d\theta}{dx} \approx \frac{\theta(0.05) - \theta(0.0)}{0.05}$$

$$\begin{aligned} \theta(0.05) &= \frac{\cosh[150(0.3-0.05)]}{\cosh[150(0.3)]} = \frac{\cosh[37.5]}{\cosh[45.0]} \\ &= \frac{9.66080 \times 10^{15}}{1.746714 \times 10^{19}} = 0.00055308 \end{aligned}$$

$$\theta(0.0) = \frac{\cosh[mL]}{\cosh[mL]} = 1.0$$

$$\left. \frac{d\theta}{dx} \right|_{\Delta x=0.05} = \frac{0.00055308 - 1.0}{0.05} = -19.9889$$

$$\left. \frac{d\theta}{dx} \right|_{\text{exact}} = \frac{1}{\cosh[mL]} \left\{ \sinh[m(L-x)] - m \right\} = \frac{-m \sinh[m(L-x)]}{\cosh[mL]}$$

$$\left. \frac{d\theta}{dx} \right|_{\text{exact}} \Big|_{x=0} = \frac{-m \sinh(mL)}{\cosh(mL)} = -150.0 \tanh(45.0) = -150.0 (1.0) = -150.$$

$$\epsilon_t = \frac{-150.0 - (-19.9889)}{-150.0} \times 100\% = 86.67\%$$

3.7 (continued)

3-7-2

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$$\left. \frac{d\theta}{dx} \right|_{\Delta x = 0.01} = \frac{\theta(0.01) - \theta(0.0)}{0.01}$$

$$\begin{aligned} \theta(0.01) &= \frac{\cosh [150(0.3 - 0.01)]}{\cosh [45.0]} = \frac{\cosh (43.5)}{\cosh (45.0)} \\ &= \frac{3.89744 \times 10^{18}}{1.746714 \times 10^{19}} = 0.22313 \end{aligned}$$

$$\left. \frac{d\theta}{dx} \right|_{\Delta x = 0.01} = \frac{0.22313 - 1.0}{0.01} = -77.687$$

$$\epsilon_t = \frac{-150.0 - (-77.687)}{-150.0} \times 100\% = 48.21\%$$

$$a \frac{d^2 T}{dx^2} + b(c - T) = 0$$

Derive discretization equation by integrating over the typical "Tp" control volume shown in the diagram.

$$\int_V a \frac{d^2 T}{dx^2} dV + \int_V b(c - T) dV = 0$$

$$a \int_A \int_W^e \frac{d}{dx} \left(\frac{dT}{dx} \right) dx dA + \int_A \int_W^e (bc - bT) dx dA = 0$$

For constant cross-sectional area A and values assumed constant over the cv. faces and simplifying

$$aA \left[\left(\frac{dT}{dx} \right)_e - \left(\frac{dT}{dx} \right)_w \right] + bcA \int_W^e dx - bA \int_W^e T dx = 0$$

Assume a piecewise linear profile for T for $\frac{dT}{dx}$ terms.

$$\Rightarrow \left(\frac{dT}{dx} \right)_e \approx \frac{(T_E - T_P)}{(\delta x)_e} \quad \text{and} \quad \left(\frac{dT}{dx} \right)_w \approx \frac{(T_P - T_W)}{(\delta x)_w}$$

Assume a stepwise profile for the $\int T dx$ term

$$\int_w^e T dx \approx T_p \int_w^e dx$$

$$\Rightarrow aA \left[\frac{(T_E - T_p)}{(\delta x)_e} - \frac{(T_p - T_w)}{(\delta x)_w} \right] + bcA(\Delta x) - bAT_p(\Delta x) = 0$$

$$\Rightarrow \frac{aA}{(\delta x)_e} T_E + \frac{aA}{(\delta x)_w} T_w - \left(\frac{aA}{(\delta x)_e} + \frac{aA}{(\delta x)_w} \right) T_p + bcA(\Delta x) - bA(\Delta x)T_p = 0$$

$$\Rightarrow A \left(\frac{a}{(\delta x)_e} + \frac{a}{(\delta x)_w} + b(\Delta x) \right) T_p = \frac{Aa}{(\delta x)_e} T_E + \frac{Aa}{(\delta x)_w} T_w + bcA(\Delta x)$$

dividing through by A yields

$$\left[\frac{a}{(\delta x)_e} + \frac{a}{(\delta x)_w} + b(\Delta x) \right] T_p = \frac{a}{(\delta x)_e} T_E + \frac{a}{(\delta x)_w} T_w + bc(\Delta x)$$

$$\Rightarrow \begin{cases} a_p = a_E + a_w + b(\Delta x) \\ a_E = \frac{a}{(\delta x)_e} \\ a_w = \frac{a}{(\delta x)_w} \\ b_p = bc(\Delta x) \end{cases}$$

(or with A multiplying all terms)

$$(a) \underbrace{\int_V \frac{d^2\Phi}{dx^2} dV}_I - \underbrace{\int_V D x^2 \Phi dV}_{II} = 0$$

Assume piecewise linear profile for term I

$$I = A_e \frac{d\Phi}{dx}|_e - A_w \frac{d\Phi}{dx}|_w = A_e \frac{(\Phi_E - \Phi_p)}{\Delta x} - A_w \frac{(\Phi_p - \Phi_w)}{\Delta x}$$

$$= \frac{A}{\Delta x} \Phi_E + \frac{A}{\Delta x} \Phi_w - \frac{2A}{\Delta x} \Phi_p$$

$$II = -D \int_A \int_w^e x^2 \Phi dx dA$$

Assume stepwise profile for Φ in term II

$$\Rightarrow II = -D \int_A \Phi_p \int_w^e x^2 dx dA = -D \int_A \Phi_p \frac{x^3}{3} \Big|_w^e dA$$

$$II = -D \int_A \Phi_p \frac{(x_e^3 - x_w^3)}{3} dA = -\frac{DA_p}{3} \Phi_p (x_e^3 - x_w^3)$$

$$II = -\frac{DA_p}{3} (x_e^3 - x_w^3) \Phi_p$$

Gather terms,

$$\frac{A}{\Delta x} \Phi_E + \frac{A}{\Delta x} \Phi_w - \frac{2A}{\Delta x} \Phi_p - \frac{DA_p}{3} (x_e^3 - x_w^3) \Phi_p = 0$$

$$\left[\frac{2A}{\Delta x} + \frac{DA_p}{3} (x_e^3 - x_w^3) \right] \Phi_p = \frac{A}{\Delta x} \Phi_E + \frac{A}{\Delta x} \Phi_w$$

$$a_p = (2A/\Delta x) + DA_p(x_e^3 - x_w^3)/3$$

$$a_E = A/\Delta x$$

$$a_w = A/\Delta x$$

$$b_p = 0$$