

(CONTINUED)

$$(q_n)_7 = \frac{k_n A_n}{(\delta y)_n}$$

$$k_n = \frac{k_p k_N}{f_n k_p + (1-f_n) k_N}$$

$$k_p = k_c$$
$$k_N = k_B$$

$$k_n = \frac{k_c k_B}{[f_n k_c + (1-f_n) k_B]} \quad f_n = 0.62500$$

$$(q_n)_7 = \frac{(64)(4)}{[(0.62500)64 + (1-0.62500)(4)]} = 6.1687 \left(\frac{W}{mK} \right)$$

$$A_n = 0.2(1) = 0.2 \text{ (m}^2\text{)}$$

$$(q_n)_7 = \frac{6.1687 (0.20)}{0.40} = 3.0844$$

$$(\delta y)_n = 0.4 \text{ (m)}$$

$$(q_p)_7 = 21.333 + 96.00 + 42.667 + 3.0844 = 163.0844 \leftarrow$$

$$(b_p)_7 = 0.0$$

$$(c) \quad (q_p)_6 T_6 = (q_w)_6 T_5 + (q_E)_6 T_7 + (q_S)_6 T_2 + (q_N)_6 T_{10} + 0$$

$$56.2312 T_6 = 8.000 (320) + 21.333 T_7 + 21.333 (310) + 5.5652 (380)$$

$$56.2312 T_6 = 21.333 T_7 + 11,288.0 \quad (1)$$

$$(q_p)_7 T_7 = (q_w)_7 T_6 + (q_E)_7 T_8 + (q_S)_7 T_3 + (q_N)_7 T_{11} + 0$$

$$163.0844 T_7 = 21.333 T_6 + 96.00 (370) + 42.667 (340) + 3.0844 (410)$$

$$163.0844 T_7 = 21.333 T_6 + 51,291.4 \quad (2)$$

CONTINUED

$$(d) \quad 56.2312 T_6 = 21.333 T_7 + 11,288.0 \quad (1)$$

$$163.0844 T_7 = 21.333 T_6 + 51,291.4 \quad (2)$$

From (1)

$$T_6 = \frac{21.333 T_7}{56.2312} + \frac{11,288.0}{56.2312}$$

$$T_6 = 0.37938 T_7 + 200.743 \quad (3)$$

Substitute (3) into (2)

$$163.0844 T_7 = 21.333 (0.37938 T_7 + 200.743) + 51,291.4$$

$$(163.0844 - 21.333(0.37938)) T_7 = 21.333(200.743) + 51,291.4$$

$$154.991 T_7 = 55,573.85$$

$$T_7 = \underline{358.56} \text{ [K]} \quad \leftarrow$$

$$T_6 = 0.37938 (358.56) + 200.743 = 336.77 \text{ [K]} \leftarrow$$

$$T_6 = 336.77 \text{ [K]} \quad \leftarrow$$

$$T_7 = 358.56 \text{ [K]} \quad \leftarrow$$

- 2D Steady Conduction • no source term
- composite
- Uniform grid spacing but $\Delta x \neq \Delta y$
- ($A_n = A_s = \Delta x$ $A_e = A_w = \Delta y$)
- $P = k$

Eqs (15.7) to (15.10) simplify in this case to

$$\left[\frac{k_e A_e}{(\Delta x)_e} + \frac{k_w A_w}{(\Delta x)_w} + \frac{k_n A_n}{(\Delta y)_n} + \frac{k_s A_s}{(\Delta y)_s} \right] T_p = \frac{k_e A_e}{(\Delta x)_e} T_E + \frac{k_w A_w}{(\Delta x)_w} T_W + \frac{k_n A_n}{(\Delta y)_n} T_N + \frac{k_s A_s}{(\Delta y)_s} T_S$$

$$q_p = q_E + q_W + q_N + q_S \quad b_p = 0$$

(a) • cv. for T_1 $k_e = k_w = k_n = k_s = k_A = 2 \text{ (W/mK)}$

$$(\Delta x)_w = \frac{\Delta x}{2} \quad (\Delta y)_s = \frac{\Delta y}{2}$$

$$(q_E)_1 = \frac{k_A \Delta y}{\Delta x} = \frac{2(0.1)}{0.4} = 0.5$$

$$(q_W)_1 = \frac{k_A \Delta x}{\Delta y} = \frac{2(0.4)}{0.1} = 8$$

$$(q_W)_1 = \frac{k_A \Delta y}{\frac{\Delta x}{2}} = \frac{2(0.1)}{0.2} = 1.0$$

$$(q_S)_1 = \frac{k_A (\Delta x)}{\frac{\Delta y}{2}} = \frac{2(0.4)}{0.05} = 16$$

$$(q_p)_1 = 0.5 + 1.0 + 8 + 16 = 25.5$$

B.C. $T_W = T_L$ $T_S = T_2$ (by zero gradient)

$$25.5 T_1 = 0.5 T_2 + T_L + 8 T_S + 16 T_1$$

$$\boxed{9.5 T_1 = 0.5 T_2 + T_L + 8 T_S}$$

• cv for T_2 $q_{W2} = q_{E1} = 0.5$

by inspection $q_{S2} = q_{S1} = 16$

$$(k_n)_2 = \frac{2 k_A k_B}{(k_A + k_B)} = \frac{2(2)(48)}{(2+48)} = 3.84 \text{ (W/mK)}$$

$$(k_e)_2 = \frac{2(k_A k_B)}{(k_A + k_B)} = 3.84 \text{ (W/mK)}$$

$$(Q_H)_2 = \frac{(3.89)(0.4)}{0.1} = 15.36$$

$$(Q_E)_2 = \frac{(3.89)(0.1)}{(0.4)} = 0.96$$

$$(Q_p)_2 = 0.5 + 0.96 + 15.36 + 16 = 32.82$$

$$32.82 T_2 = 0.5 T_1 + 0.96 T_3 + 15.36 T_6 + 16 T_2$$

Insulated
boiler
 $T_5 = T_6$

$$16.82 T_2 = 0.5 T_1 + 0.96 T_3 + 15.36 T_6$$

(b) Substitute known T values

$$9.5 T_1 = 0.5 T_2 + 500 + 8(425.70)$$

$$9.5 T_1 = 0.5 T_2 + 3905.60$$

(3-1)

$$16.82 T_2 = 0.5 T_1 + 0.96(359.00) + 15.36(382.06)$$

$$16.82 T_2 = 0.5 T_1 + 6213.1$$

(3-2)

(c) Solve Eqs (3-1) & (3-2)

$$\text{From (3-1)} \quad T_1 = \frac{0.5}{9.5} T_2 + \frac{3905.60}{9.5} \quad (3-3)$$

Substitute (3-3) into (3-2)

$$16.82 T_2 = 0.5 \left(\frac{0.5}{9.5} T_2 + \frac{3905.60}{9.5} \right) + 6213.1$$

$$\left(\frac{16.82 - 0.25}{9.5} \right) T_2 = \frac{0.5(3905.60)}{9.5} + 6213.1$$

$$16.793 T_2 = 6418.7 \quad \rightarrow \quad T_2 = \underline{382.22 \text{ (K)}}$$

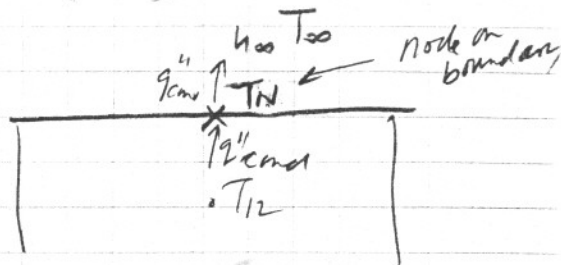
$$T_1 = \frac{0.5}{9.5} (382.22) + \frac{3905.60}{9.5} = \underline{431.23 \text{ (K)}}$$

(d) cv for T_{12} $(k_e)_{12} = (k_w)_{12} = (k_n)_{12} = k_c = 12 \text{ (W/mK)}$
 $(k_s)_{12} = \frac{2 k_B k_c}{(k_B + k_c)} = \frac{2(48)(12)}{(48+12)} = 19.2 \text{ (W/mK)}$

Top boundary condition for 12

$$q_{cond}'' = q_{conv}''$$

$$-k_c(T_N - T_{12}) = h_{\infty} \frac{\Delta y}{2} (T_N - T_{\infty})$$



$$-k_c T_N + k_c T_{12} = \frac{h_{\infty} \Delta y}{2} T_N - \frac{h_{\infty} \Delta y}{2} T_{\infty}$$

$$\left(k_c + \frac{h_{\infty} \Delta y}{2}\right) T_N = k_c T_{12} + \frac{h_{\infty} \Delta y}{2} T_{\infty}$$

$$T_N = \frac{k_c}{\left(k_c + \frac{1}{2} h_{\infty} \Delta y\right)} T_{12} + \frac{\frac{1}{2} h_{\infty} \Delta y}{\left(k_c + \frac{1}{2} h_{\infty} \Delta y\right)} T_{\infty}$$

Use this equation for T_N in T_{12} equation

$$(q_E)_{12} = 12 \left(\frac{0.1}{0.14}\right) = 3 \quad (q_W)_{12} = 12 \left(\frac{0.1}{0.2}\right) = 6$$

$$(q_S)_{12} = 19.2 \left(\frac{0.4}{0.1}\right) = 76.8 \quad (q_N)_{12} = 12 \left(\frac{0.4}{0.05}\right) = 96$$

$$q_p = 3 + 6 + 76.8 + 96 = 181.8$$

$$181.8 T_{12} = 3 T_{11} + 6 T_R + 76.8 T_g + 96 T_N$$

$$T_N = \frac{12}{(12 + \frac{1}{2}(40)(0.1))} T_{12} + \frac{\frac{1}{2}(40)(0.1)}{[12 + \frac{1}{2}(40)(0.1)]} 400$$

$$T_N = 0.85714 T_{12} + 57.1429$$

$$181.8 T_{12} = 3(366.69) + 6(300) + 76.8(330.28) + 96(0.85714 T_{12} + 57.1429)$$

$$\Rightarrow 99.515 T_{12} = 33751.29$$

$$T_{12} = \underline{\underline{339.16 \text{ [K]}}}$$

$$(a) \quad T_L = T_1 + \frac{q_L'' \Delta x}{2k}$$

$$T_L = T_1 + \frac{(1000)(0.2)}{2(35)} = T_1 + 2.85714$$

$$\boxed{T_L = T_1 + 2.85714}$$

(b) Substitute T_L equation into previous algebraic equation for T_1

$$525 T_1 = 350 \{ T_1 + 2.85714 \} + 175 T_2 + 111$$

$$525 T_1 = 350 T_1 + 1000 + 175 T_2 + 111$$

$$\boxed{175 T_1 = 175 T_2 + 1111}$$

$$(c) \quad T_R = \frac{1}{\left(1 + \frac{h_{\infty} \Delta x}{2k}\right)} T_3 + \frac{\left(\frac{h_{\infty} \Delta x}{2k}\right)}{\left(1 + \frac{h_{\infty} \Delta x}{2k}\right)} T_{\infty}$$

$$T_R = \frac{1}{\left(1 + \frac{70(0.2)}{2(35)}\right)} T_3 + \frac{\frac{70(0.2)}{2(35)} 300}{\left(1 + \frac{70(0.2)}{2(35)}\right)}$$

$$T_R = \frac{1}{1.2} T_3 + \frac{0.2}{1.2} 300$$

$$\boxed{T_R = 0.8333 T_3 + 50}$$

(d) substitute T_R equation into previous algebraic equation

for T_3

$$525 T_3 = 175 T_2 + 350 \{ 0.8333 T_3 + 50 \} + 111$$

$$525 T_3 = 175 T_2 + 291.666 T_3 + 17,500 + 111$$

$$\boxed{233.33 T_3 = 175 T_2 + 17,611}$$

(e) The new equation set is

$$175 T_1 = 175 T_2 + 1111 \quad (1)$$

$$350 T_2 = 175 T_1 + 175 T_3 + 111 \quad (2)$$

$$233.33 T_3 = 175 T_2 + 17,611 \quad (3)$$

which in matrix form is

$$\begin{bmatrix} 175 & -175 & 0 \\ -175 & 350 & -175 \\ 0 & -175 & -233.33 \end{bmatrix} \begin{Bmatrix} T_1 \\ T_2 \\ T_3 \end{Bmatrix} = \begin{bmatrix} 1111 \\ 111 \\ 17,611 \end{bmatrix} \begin{matrix} \text{row 1} \\ \text{row 2} \\ \text{row 3} \end{matrix}$$

Solving: Add rows 1 & 2:

$$175 T_2 - 175 T_3 = 1222 \quad (4)$$

$$\text{add (4) + row 5:} \quad 58.33 T_3 = 18,833 \quad (5)$$

$$T_3 = \underline{322.87}$$

$$\Rightarrow T_2 = \frac{1222 + 175(322.87)}{175}$$

$$T_2 = \underline{329.85}$$

$$T_1 = \frac{175(329.85) + 1111}{175}$$

$$T_1 = \underline{336.20}$$

$$\begin{Bmatrix} T_1 \\ T_2 \\ T_3 \end{Bmatrix} = \begin{Bmatrix} 336.20 \\ 329.85 \\ 322.87 \end{Bmatrix}$$

5.11

5-11-1

(a)

$$k_e = k_w = k = 70 \text{ (W/mK)}$$

$$A_e = A_w = A = 1 \text{ (m}^2\text{)}$$

$$\Delta x = 4/3 = 0.6/3 = 0.2 \text{ (m)}$$

$$T_p = T_1$$

$$T_w = T_L$$

$$T_e = T_2$$

$$(\delta x)_w = \frac{\Delta x}{2} = 0.1 \text{ (m)}$$

$$(\delta x)_e = \Delta x = 0.2 \text{ (m)}$$

Equation 2 ($i=1$)

$$\left(\frac{70(1)}{0.1} + \frac{70(1)}{0.2} \right) T_1 = \frac{70(1)}{0.1} T_L + \frac{70(1)}{0.2} T_2 + 1110(1)(0.2)$$

$$1050 T_1 = 700 T_L + 350 T_2 + 222$$

$$i=2 \quad T_p = T_2 \quad (T_w = T_1 \quad T_e = T_3)$$

$$\left(\frac{70(1)}{0.2} + \frac{70(1)}{0.2} \right) T_2 = \frac{70(1)}{0.2} T_1 + \frac{70(1)}{0.2} T_3 + 1110(1)0.2$$

$$700 T_2 = 350 T_1 + 350 T_3 + 222$$

$$i=3 \quad T_p = T_3 \quad (T_w = T_2 \quad T_e = T_R)$$

$$\left(\frac{70(1)}{0.2} + \frac{70(1)}{0.1} \right) T_3 = \frac{70(1)}{0.2} T_2 + \frac{70(1)}{0.1} T_R + 1110(1)(0.2)$$

$$1050 T_3 = 350 T_2 + 700 T_R + 222$$

$$1050 T_1 = 700 T_L + 350 T_2 + 222$$

$$700 T_2 = 350 T_1 + 350 T_3 + 222$$

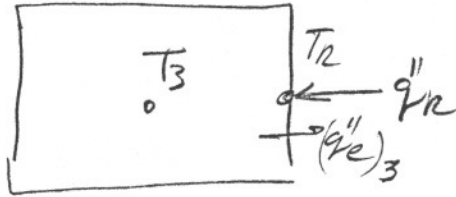
$$1050 T_3 = 350 T_2 + 700 T_R + 222$$

CONTINUED

(b) Background

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At the right boundary



$$(q''_e)_3 = -k \frac{dT}{dx} \Big|_e = -k \frac{(T_r - T_3)}{\left(\frac{\Delta x}{2}\right)} = -\frac{2k}{\Delta x} (T_r - T_3)$$

But $q''_r = -(q''_e)_3$ so $q''_r = +\frac{2k}{\Delta x} (T_r - T_3)$

$$\Rightarrow q''_r \frac{\Delta x}{2k} = T_r - T_3$$

$$\Rightarrow T_r = T_3 + q''_r \frac{\Delta x}{2k}$$

Specific equation: $T_r = T_3 + \frac{2000(0.2)}{2(70)}$

$$T_r = T_3 + 2.8571$$

(c) Substitute $T_r = 400$ in T_1 equation

$$1050 T_1 = 700(400) + 350 T_2 + 222$$

$$\Rightarrow 1050 T_1 = 350 T_2 + 280222$$

Equation for T_2 is unchangedSubstitute for T_r in T_3 equation:

$$1050 T_3 = 350 T_2 + 700(T_3 + 2.8571) + 222$$

$$\Rightarrow 350 T_3 = 350 T_2 + 2222$$

Modified equation set

$$1050 T_1 = 350 T_2 + 280222 \quad (1)$$

$$700 T_2 = 350 T_1 + 350 T_3 + 222 \quad (2)$$

$$350 T_3 = 350 T_2 + 2222 \quad (3)$$

Solution

$$\text{Eqn (1)} - \text{Eqn (3)}$$

$$1050 T_1 - 350 T_3 = 278,000 \quad (4)$$

$$\text{Eqn (2)} + 2 \text{Eqn (3)}$$

$$\begin{aligned} 700 T_2 + 700 T_3 &= 350 T_1 + 350 T_3 + 222 + \\ &\quad + 700 T_2 + 4444 \end{aligned}$$

$$-350 T_1 + 350 T_3 = 4666 \quad (5)$$

$$\text{Eqn (4)} + \text{Eqn (5)}$$

$$700 T_1 = 282,666$$

$$T_1 = 403.81 \text{ [K]}$$

$$\Rightarrow T_3 = \frac{1}{350} (4666 + 350 (403.81))$$

$$T_3 = 417.14 \text{ [K]}$$

$$T_2 = \frac{1}{700} (350 (403.81) + 350 (417.14) + 222)$$

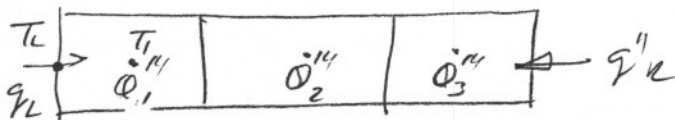
$$T_2 = 410.79 \text{ [K]}$$

CHECK

$$\begin{aligned}
 1050 (403.81) &\stackrel{?}{=} 350 (410.79) + 280222 && \checkmark \\
 700 (410.79) &\stackrel{?}{=} 350 (403.81) + 350 (417.14) + 222 && \checkmark \\
 350 (417.14) &\stackrel{?}{=} 350 (410.79) + 2222 && \checkmark
 \end{aligned}$$

(d)

Overall energy balance:



$$\dot{E}_{in} + \dot{E}_{gen} = \dot{E}_{out}$$

$$q_L'' A + [\dot{Q}_1'' A \Delta x + \dot{Q}_2'' A \Delta x + \dot{Q}_3'' A \Delta x] = -q_R'' A$$

$$-k \frac{(T_1 - T_L)}{\left(\frac{\Delta x}{2}\right)} + (\dot{Q}_1'' + \dot{Q}_2'' + \dot{Q}_3'') \Delta x = -q_R'' A$$

$$\frac{-70 (403.81 - 400)}{0.1} + (3330) (0.2) \stackrel{?}{=} -2000$$

$$-2667 + 666 \stackrel{?}{=} -2000$$

$$-2001 \stackrel{?}{=} -2000$$

✓ balances to 0.05%

$$(a) \underbrace{\int_t^{t+\Delta t} \int_V \frac{\partial (\rho T)}{\partial t} dV dt}_{\text{I}} = \underbrace{\int_t^{t+\Delta t} \int_V \frac{\partial (\rho T)}{\partial x} \left(\frac{\partial T}{\partial x} \right) dV dt}_{\text{II}} + \underbrace{\int_t^{t+\Delta t} \int_V \frac{\partial (\rho T)}{\partial y} \left(\frac{\partial T}{\partial y} \right) dV dt}_{\text{III}}$$

$$\text{I} = \int_t^{t+\Delta t} \int_V \left[\frac{\partial (\rho T)}{\partial t} \right]_p dV dt = \rho_p (\text{Vol})_p \int_t^{t+\Delta t} \frac{\partial (T_p)}{\partial t} dt$$

(assuming $T \approx T_p$ and $\rho = \text{constant}$)

$$\boxed{\text{I} = \rho_p (\text{Vol})_p (T_p^n - T_p^0)}$$

$$\text{II} = \int_t^{t+\Delta t} \int_A \left[\Gamma_e \frac{\partial T}{\partial x} \Big|_e - \Gamma_w \frac{\partial T}{\partial x} \Big|_w \right] dA dt = \int_t^{t+\Delta t} \left[\Gamma_e A_e \frac{\partial T}{\partial x} \Big|_e - \Gamma_w A_w \frac{\partial T}{\partial x} \Big|_w \right] dt$$

(assuming $\frac{\partial T}{\partial x}$ constant over each w & e face)

$$\frac{\partial T}{\partial x} \Big|_e \approx \frac{(T_E - T_p)}{(\delta x)_e}$$

$$\frac{\partial T}{\partial x} \Big|_w \approx \frac{(T_p - T_w)}{(\delta x)_w}$$

} piecewise linear
profile assumed

$$\text{II} = \int_t^{t+\Delta t} \left[\frac{\Gamma_e A_e}{(\delta x)_e} (T_E - T_p) - \frac{\Gamma_w A_w}{(\delta x)_w} (T_p - T_w) \right] dt$$

Using the Fully Explicit time weight directly

$$(ft = 0 \text{ so } T_i \approx T^{\circ}) \Rightarrow \int_t^{t+\Delta t} T dt = T^{\circ} \Delta t$$

$$II = \left[\frac{\Gamma_e A_e}{(\delta x)_e} (T_E^{\circ} - T_p^{\circ}) - \frac{\Gamma_w A_w}{(\delta x)_w} (T_p^{\circ} - T_w^{\circ}) \right] \Delta t$$

$$III = \int_t^{t+\Delta t} \left[\Gamma_n A_n \frac{\partial T}{\partial y}_n - \Gamma_s A_s \frac{\partial T}{\partial y}_s \right] dt$$

$$\frac{\partial T}{\partial y}_n = \frac{(T_N - T_p)}{(\delta y)_n}$$

$$\frac{\partial T}{\partial y}_s = \frac{(T_p - T_s)}{(\delta y)_s}$$

piecewise linear
profile assumed

$$III = \int_t^{t+\Delta t} \left[\frac{\Gamma_n A_n}{(\delta y)_n} (T_N - T_p) - \frac{\Gamma_s A_s}{(\delta y)_s} (T_p - T_s) \right] dt$$

Using Fully Explicit again

$$III = \left[\frac{\Gamma_n A_n}{(\delta y)_n} (T_N^{\circ} - T_p^{\circ}) - \frac{\Gamma_s A_s}{(\delta y)_s} (T_p^{\circ} - T_s^{\circ}) \right] \Delta t$$

Assembling

$$SP^{(n)}_p (T_p^n - T_p^{\circ}) = \left[\frac{\Gamma_e A_e}{(\delta x)_e} (T_E^{\circ} - T_p^{\circ}) - \frac{\Gamma_w A_w}{(\delta x)_w} (T_p^{\circ} - T_w^{\circ}) \right] \Delta t$$

$$+ \left[\frac{\Gamma_n A_n}{(\delta y)_n} (T_N^{\circ} - T_p^{\circ}) - \frac{\Gamma_s A_s}{(\delta y)_s} (T_p^{\circ} - T_s^{\circ}) \right] \Delta t$$

DIVIDE BY Δt AND GATHER TERMS

$$\frac{\rho_p (Vol)_p}{\Delta t} (T_p^n - T_p^o) = \frac{\Gamma_e A_e}{(\delta x)_e} T_E^o + \frac{\Gamma_w A_w}{(\delta x)_w} T_W^o + \frac{\Gamma_n A_n}{(\delta y)_n} T_N^o + \frac{\Gamma_s A_s}{(\delta y)_s} T_S^o$$

$$- \left(\frac{\Gamma_e A_e}{(\delta x)_e} + \frac{\Gamma_w A_w}{(\delta x)_w} + \frac{\Gamma_n A_n}{(\delta y)_n} + \frac{\Gamma_s A_s}{(\delta y)_s} \right) T_p^o$$

letting $\frac{\Gamma_e A_e}{(\delta x)_e} = D_e$ $\frac{\Gamma_w A_w}{(\delta x)_w} = D_w$ $\frac{\Gamma_n A_n}{(\delta y)_n} = D_n$ $\frac{\Gamma_s A_s}{(\delta y)_s} = D_s$

$$\begin{aligned} \left(\frac{\rho_p (Vol)_p}{\Delta t} \right) T_p^n &= \phi T_w^n + \phi T_E^n + \phi T_N^n + \phi T_S^n \\ &+ [D_e T_E^o + D_w T_W^o + D_n T_N^o + D_s T_S^o] \\ &+ [-(D_e + D_w + D_n + D_s) + \frac{\rho_p (Vol)_p}{\Delta t}] T_p^o \end{aligned}$$

$$a_p = \frac{\rho_p (Vol)_p}{\Delta t}$$

$$q_E = q_W = q_N = q_S = 0$$

$$\begin{aligned} b_p &= (D_e T_E^o + D_w T_W^o + D_n T_N^o + D_s T_S^o) + \\ &+ [-(D_e + D_w + D_n + D_s) + \frac{\rho_p (Vol)_p}{\Delta t}] T_p^o \end{aligned}$$

(b) For the specific problem

$$D_e = \frac{\Gamma_e A_e}{(\delta x)_e} = \frac{k}{\rho_p} \frac{\Delta y (1)}{\Delta x} \quad \frac{J}{s \cdot mK} \frac{K}{m} \frac{m}{m}$$

$$D_e = \frac{(1.4)}{800} \frac{0.02(1)}{0.08} = 0.0004375 \left[\frac{kg}{s} \right]$$

$$D_w = D_e = 0.0004375 \left[\frac{kg}{s} \right]$$

CONTINUED

$$D_n = \frac{\Gamma_n A_n}{\delta y}_n = \frac{k}{C_p} \frac{\Delta x (L)}{\Delta y} = \frac{1.4}{800} \frac{0.08 (1)}{0.02} = 0.007000 \text{ (kg/s)}$$

$$D_s = D_n = 0.007000 \text{ (kg/s)}$$

$$\dot{m}_p(\text{Vol})_p = (1400)(0.08)(0.02)(1) = 2.24 \text{ (kg)}$$

$$\frac{2.24}{\Delta t} T_p^n = 0.0004375 (T_E^o + T_W^o) + 0.007000 (T_N^o + T_S^o) \\ - \left[-0.014875 + \frac{2.24}{\Delta t} \right] T_p^o$$

(c) For $T_p^o = 375 \text{ [K]}$ $T_W^o = 400 \text{ [K]}$ $T_E^o = 450 \text{ [K]}$
 $T_S^o = 350 \text{ [K]}$ $T_N^o = 300 \text{ [K]}$

And $\Delta t = 120 \text{ [s]}$

$$T_p^n = \left(\frac{120}{2.24} \right) \left\{ 0.0004375 (450 + 400) + 0.007000 (300 + 350) \right. \\ \left. + \left[-0.014875 + \frac{2.24}{120} \right] 375 \right\}$$

$$T_p^n = 339.84 \text{ [K]}$$

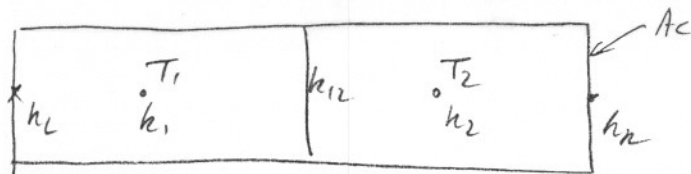
(d) Maximum time step comes from

$$\left(-0.014875 + \frac{2.24}{\Delta t} \right) \geq 0$$

$$-0.014875 \Delta t + 2.24 \geq 0$$

$$\Delta t \leq \frac{2.24}{0.014875}$$

$$\Delta t \leq 150.6 \text{ seconds}$$



$$\dot{Q}''' = 0$$

$$\Gamma = k$$

1D steady conduction

From supplementary sheets for

$$q_p T_p = q_w T_w + q_e T_e + b_p$$

$$q_w = \frac{\Gamma_w A_w}{(\delta x)_w} \quad q_e = \frac{\Gamma_e A_e}{(\delta x)_e}$$

$$q_p = q_e + q_w$$

$$b_p = 0$$

$$\dot{Q}''' = 0$$

CV #1

$$T_p = T_1 \quad T_w = T_L \quad T_e = T_2$$

$$\Gamma_w = k_w = k_L$$

$$(\delta x)_w = \Delta x / 2$$

$$A_w = A_c$$

$$\Gamma_e = k_e = k_{12}$$

$$(\delta x)_e = \Delta x$$

$$A_e = A_c$$

$$q_w = \frac{k_L A_c}{\left(\frac{\Delta x}{2}\right)}$$

$$q_e = \frac{k_{12} A_c}{\Delta x}$$

$$q_p = q_e + q_w$$

$$b_p = 0$$

$$\Rightarrow \left[\frac{2k_L A_c}{\Delta x} + \frac{k_{12} A_c}{\Delta x} \right] T_1 = \frac{2k_L A_c}{\Delta x} T_L + \frac{k_{12} A_c}{\Delta x} T_2$$

CV #2

$$\Gamma_w = k_w = k_{12}$$

$$(\delta x)_w = \Delta x$$

$$A_w = A_c$$

$$\Gamma_e = k_e = k_R$$

$$(\delta x)_e = \Delta x / 2$$

$$A_e = A_c$$

$$q_w = \frac{k_{12} A_c}{\Delta x}$$

$$q_e = \frac{k_R A_c}{\frac{\Delta x}{2}}$$

$$q_p = q_e + q_w$$

$$b_p = 0$$

CONTINUED

$$\Rightarrow \left(\frac{k_{12} A_c}{\Delta x} + \frac{2k_R A_c}{\Delta x} \right) T_2 = \frac{k_{12} A_c}{\Delta x} T_1 + \frac{2k_R A_c}{\Delta x} T_R$$

re-arrange & factor out $\left(\frac{A_c}{\Delta x}\right)$ from all terms

$$\rightarrow (2k_L + k_{12}) T_1 - k_{12} T_2 = 2k_L T_L \quad (1)$$

$$-k_{12} T_1 + (2k_R + k_{12}) T_2 = 2k_R T_R \quad (2)$$

as on the test paper.

$$b) \quad k = \text{constant} = 18.7 \text{ (W/mK)}$$

$$A_c = 0.05 \text{ (m}^2\text{)}$$

$$\Delta x = 1.87 / 2 = 0.935 \text{ (m)}$$

$$T_L = 100 \text{ (K)}$$

$$T_R = 900 \text{ (K)}$$

Equations (1) & (2) become

$$3k T_1 - k T_2 = 2k T_L$$

$$-k T_1 + 3k T_2 = 2k T_R$$

divide by k and substitute for T_L & T_R

$$\rightarrow 3T_1 - T_2 = 200 \quad (3)$$

$$-T_1 + 3T_2 = 1800 \quad (4)$$

$$(4) \rightarrow T_1 = 3T_2 - 1800 \quad (5)$$

Substitute (5) into (3)

$$3(3T_2 - 1800) - T_2 = 200$$

$$8T_2 = 5600$$

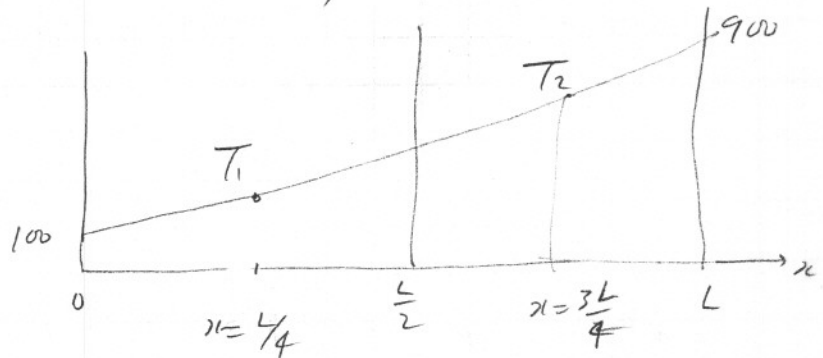
$$T_2 = 700 \text{ (K)}$$

From (5)

$$T_1 = 3(700) - 1800 = 2100 - 1800$$

$$T_1 = 300 \text{ (K)}$$

c) Analytical solution 1D steady no source terms
→ linear



$$T(x) = T_L + \frac{(T_R - T_L)}{L} x$$

$$T_1 = T\left(\frac{L}{4}\right) = T_L + \frac{(T_R - T_L)}{L} \frac{L}{4} = T_L + \frac{1}{4}(T_R - T_L)$$

$$T_1 = 100 + \frac{1}{4}(900 - 100) = 100 + \frac{800}{4} = 100 + 200 = 300$$

$$T_2 = T\left(\frac{3L}{4}\right) = T_L + \frac{3}{4}(T_R - T_L) = 100 + \frac{3}{4}(900 - 100)$$

$$T_2 = 100 + \frac{3(800)}{400} = 100 + 600 = 700 \checkmark$$

T_1 & T_2 nodal values are identical to the analytical solution.